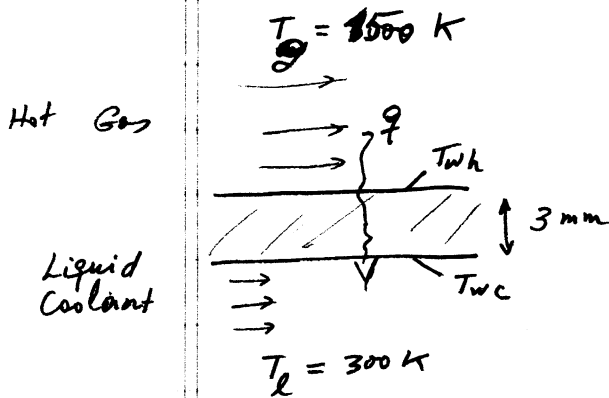


Problem 1

Consider a situation as sketched. The wall is made of steel, with a thermal conductivity $k = 40 \text{ W/m}\cdot\text{K}$. The gas is ^{air} at a pressure of 50 atm, and flows at a velocity of 700 m/s. The liquid is water, flowing at 60 m/s. The friction coefficients are estimated as $C_f = 0.0011$ on the gas side, and $C_f = 0.0033$ on the liquid side. Calculate the steady state heat flux q and the temperatures T_{wh} , T_{wc} .



Solution:

Gas side film coef.: $h_g = \frac{P_g u_g C_p S_{Tg}}{x_g} \quad S_{Tg} \approx \frac{(C_p)g}{2}$

$$P_g = \frac{P_g}{R_g T_g} = \frac{50 \times 1.013 \times 10^5}{287 \times 1500} = 11.8 \text{ kg/m}^3$$

$$C_{pg} = \frac{\gamma}{\gamma - 1} R_g = \frac{1.4}{0.4} 287 = 1004.5 \text{ J/kg}\cdot\text{K}$$

$$h_g = 11.8 \times 700 \times 1004.5 \times \frac{0.0011}{2} = 4560 \text{ W/m}^2\cdot\text{K}$$

Liquid side film coefficient: $h_l = \frac{P_l u_l C_p S_{Tl}}{x_l} \quad S_{Tl} \approx \frac{(C_p)l}{2}$

$$P_l = 1000 \text{ kg/m}^3$$

$$C_{pl} = 1 \text{ Cal/g}\cdot\text{K} = 4180 \frac{\text{J}}{\text{kg}\cdot\text{K}}$$

$$h_l = 1000 \times 60 \times 4180 \times \frac{0.0033}{2} = 414,000 \text{ W/m}^2\cdot\text{K}$$

$$q = h_g (3000 - T_{wh}) = 4560 (3000 - T_{wh})$$

$$q = 40 \frac{T_{wh} - T_{wc}}{0.003} = 13,300 (T_{wh} - T_{wc})$$

$$q = h_l (T_{wc} - 300) = 414,000 (T_{wc} - 300)$$

$$\frac{q}{A} = 3000 - T_{wh}$$

$$q = 9.10 \times 10^6 \text{ W/m}^2 \cdot \text{K}$$

and then

$$T_{wh} = 3000 - \frac{9.10 \times 10^6}{45000}$$

$$T_{wh} = 1004 \text{ K}$$

$$T_{wc} = 300 + \frac{9.10 \times 10^6}{414,000}$$

$$T_{wc} = 322 \text{ K}$$

Problem 2

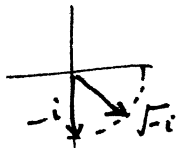
Solution

(a) Take $T = \bar{T} + \text{Re} [A e^{i(\omega t - ky)}]$ and substitute into $\frac{\partial T}{\partial t} = \alpha \frac{\partial^2 T}{\partial y^2}$. Leaving out the Re notation, we get

$$A i \omega e^{i(\omega t - ky)} = \alpha A (-k^2) e^{i(\omega t - ky)} \quad k^2 = -i \frac{\omega}{\alpha}$$

$$k = \pm \sqrt{-i \frac{\omega}{\alpha}}$$

Now $\sqrt{-i} = \frac{1-i}{\sqrt{2}}$, so $k = \pm (1-i) \sqrt{\frac{\omega}{2\alpha}}$



$$e^{-iky} = e^{\mp i(1-i) \sqrt{\frac{\omega}{2\alpha}} y} = e^{\mp (i+1) \sqrt{\frac{\omega}{2\alpha}} y}$$

$$= e^{\mp \sqrt{\frac{\omega}{2\alpha}} y} e^{\mp i \sqrt{\frac{\omega}{2\alpha}} y}$$

The first factor is exponentially divergent in y if the lower sign is chosen, so we take the upper sign:

$$T = \bar{T} + \text{Re} [A e^{i(\omega t - \sqrt{\frac{\omega}{2\alpha}} y)}]$$

If $A = A_R + i A_I$, this is $T = \bar{T} + \Delta T e^{-\sqrt{\frac{\omega}{2\alpha}} y} [A_R \cos(\dots) - A_I \sin(\dots)]$.
 Since we want $T(y=0) = \bar{T} + \Delta T \sin \omega t$, we take

$$A_R = 0 \quad ; \quad A_I = -\Delta T$$

$$T = \bar{T} + \Delta T e^{-\sqrt{\frac{\omega}{2\alpha}} y} \sin(\omega t - \sqrt{\frac{\omega}{2\alpha}} y)$$

(b) With $\Delta T = 20 \text{ K}$, if we want the oscillation amplitude to be 1 K only we need

$$e^{-\sqrt{\frac{\omega}{2\alpha}} y} = 0.05 \quad y = \sqrt{\frac{2\alpha}{\omega}} \ln 20$$

We have for the soil $\alpha = \frac{k}{\rho c} = \frac{1.6}{2000 \times 2000} = 4 \times 10^{-7} \text{ m}^2/\text{s}$, and $\omega = 1.99 \times 10^{-7} \text{ s}^{-1}$, so $\sqrt{\frac{2\alpha}{\omega}} = \sqrt{\frac{2 \times 4 \times 10^{-7}}{1.99 \times 10^{-7}}} \ln 20 \approx \underline{6.0 \text{ m}}$

Also then $\sqrt{\frac{\omega}{2\alpha}} y = \ln 20 \approx 3.0$, and this is, in radians, the delay in reaching peak temperature. In days, $\delta t = 3.0 \frac{365}{2\pi} = 174 \text{ days} = 5.7 \text{ months}$
 (peak T reached in mid-winter) -